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UTILITY PATENT
APPLICATION TRANSMITTAL LETTER

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Box PATENT APPLICATION
Assistant Commissioner for Patents
Washington, D.C. 20231

Sir:

Enclosed for filing is the utility patent application of Ingrid REINECK, Torbjörn SELINDER, Anders PIIRHONEN, and Gregor KULLANDER for COATED GROOVING OR PARTING INSERT.

Also enclosed are:

- ☒ One sheet(s) of ☒ formal ☐ informal drawing(s);
- ☒ a claim for foreign priority under 35 U.S.C. §§ 119 and/or 365 is ☒ hereby made to 9802488-8 filed in Sweden on July 9, 1998; ☒ in the declaration;
- ☐ a certified copy of the priority document;
- ☐ a Constructive Petition for Extensions of Time;
- ☐ _____ statement(s) claiming small entity status;
- ☐ an Assignment document;
- ☐ an Information Disclosure Statement; and
- ☐ Other: _____

The declaration of the inventor(s) ☐ also is enclosed ☒ will follow.

- ☒ Please amend the specification by inserting before the first line the sentence --This application claims priority under 35 U.S.C. §§119 and/or 365 to Swedish Application No. 9802488-8 filed in Sweden on July 9, 1998; the entire content of which is hereby incorporated by reference.--

The filing fee has been calculated as follows [] and in accordance with the enclosed preliminary amendment:

CLAIMS					
	NO. OF CLAIMS		EXTRA CLAIMS	RATE	FEE
Basic Application Fee					\$760.00
Total Claims	20	MINUS 20 =	0	x \$18.00	
Independent Claims	2	MINUS 3 =	0	x \$78.00	
If multiple dependent claims are presented, add \$260.00					
Total Application Fee					\$760.00
If verified Statement claiming small entity status is enclosed, subtract 50% of Total Application Fee					
Add Assignment Recording Fee of \$40.00 if Assignment document is enclosed					
TOTAL APPLICATION FEE DUE					\$760.00

☒ A check in the amount of \$ 760.00 is enclosed for the fee due.

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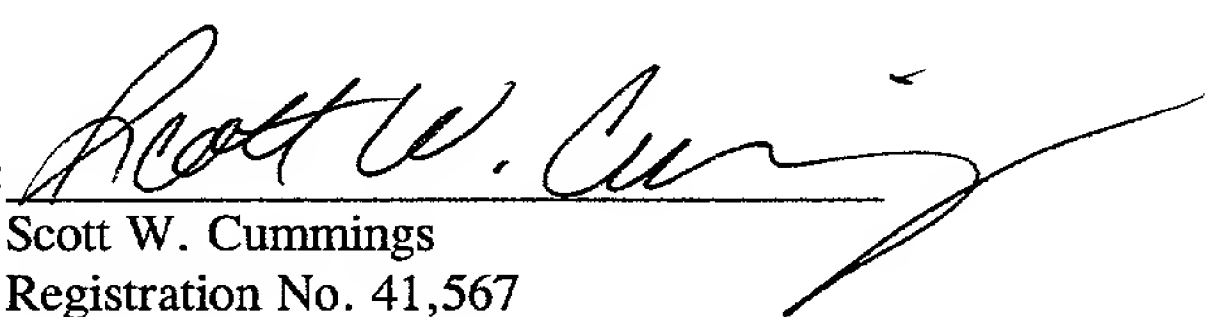
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The Commissioner is hereby authorized to charge any appropriate fees under 37 C.F.R. §§ 1.16, 1.17 and 1.21 that may be required by this paper, and to credit any overpayment, to Deposit Account No. 02-4800. This paper is submitted in triplicate.

Respectfully submitted,

BURNS, DOANE, SWECKER & MATHIS, L.L.P.

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COATED GROOVING OR PARTING INSERT

Field of the Invention

The present invention relates to a coated cemented carbide body. The present invention further relates to a coated cutting tool insert useful for grooving
5 or severing steel components such as steel or stainless steel tubes and bars.

Background of the Invention

When steel or stainless steel tubes or bars are severed using an appropriate coated cutting tool or cutting tool insert, the cutting edge is frictionally heated to a high temperature with the consequence that the material being cut becomes welded
10 onto the cutting edge of the cutting tool insert. As a result, the coating can flake and small cemented carbide chips can be torn out of the cutting tool or cutting tool insert substrate body.

On the other hand, for grooving of the same materials, a high coating wear resistance in combination with a stiff substrate material is required. Finding a
15 cutting tool material that effectively fulfils both these requirements is a challenge.

So far it has been very difficult to improve all tool properties simultaneously. Commercial cemented carbide grades have therefore been optimised with respect to one or few of the wear types and hence to specific application areas.

20 Swedish patent application 9602413-8 discloses a coated cutting insert particularly suited for wet turning or grooving stainless steel components. The inserts are characterised by a cemented carbide body consisting of WC-Co and cubic carbides coated by one layer of $\text{TiC}_x\text{N}_y\text{O}_z$ with columnar grains, one layer of smooth, fine grained $\kappa\text{-Al}_2\text{O}_3$, and preferably an outer layer of TiN.

25 Swedish patent application 9504304-8 discloses a coated cutting insert particularly useful for wet and dry milling of low and medium alloyed steels. The

insert is characterised by a cemented carbide substrate consisting of Co-WC and cubic carbides, a coating including a layer of $\text{TiC}_x\text{N}_y\text{O}_z$ with columnar grains, a layer of smooth, fine grained $\kappa\text{-Al}_2\text{O}_3$ and preferably an outer layer of TiN.

Summary of the Invention

5 According to the present invention, a combination of the cemented carbide substrates, coatings and insert styles has been developed which gives rise to excellent cutting performance in grooving as well as severing of steel or stainless steel.

10 According to the principles of the present invention, a cutting tool insert is provided which comprises:

 a cemented carbide body comprising

 6-15 weight % Co, 0.2-1.8 weight % cubic carbides of Ti, Ta and/or Nb, a highly W-alloyed binder phase with a CW-ratio of 0.78-0.93, and the balance WC; and

15 a coating comprising

 a first innermost layer of $\text{TiC}_x\text{N}_y\text{O}_z$ wherein $x+y+z=1$, the first layer having a thickness of 0.1-1.5 μm and equiaxed grains with size $<0.5 \mu\text{m}$,

20 a second layer of $\text{TiC}_x\text{N}_y\text{O}_z$ wherein $x+y+z=1$, the second layer having a thickness of 0.4-3.9 μm , preferably 1.5-3.0 μm , with columnar grains with an average diameter of 0.1-5.0 μm ,

 a third layer of a smooth fine-grained $\kappa\text{-Al}_2\text{O}_3$ layer with a thickness of 0.5-5.5 μm , and

25 the total thickness of the first innermost $\text{TiC}_x\text{N}_y\text{O}_z$ and the second $\text{TiC}_x\text{N}_y\text{O}_z$ layer is 0.5-4.0 μm , and the total thickness of all layers is 2.0-6.0 μm , preferably 3.0-5.0 μm .

Further according to the present invention, a method of making a cutting tool insert comprising a WC-Co-based cemented carbide body with a highly W-alloyed binder phase and a CW-ratio of 0.78-0.93, the method comprising coating the body by:

5 forming a first innermost layer of $\text{TiC}_x\text{N}_y\text{O}_z$ with a CVD-based technique, wherein $x+y+z=1$, the first layer having a thickness of 0.1-1.5 μm and equiaxed grains with a size $< 0.5 \mu\text{m}$,

 forming a second layer of $\text{TiC}_x\text{N}_y\text{O}_z$ by a MTCVD-technique, wherein $x+y+z=1$, the second layer having a thickness of 0.4-3.9 μm and columnar grains
10 with an average diameter of 0.1-5.0 μm ,

 forming a third layer of a smooth $\kappa\text{-Al}_2\text{O}_3$ having a thickness of 0.5-5.5 μm , and

 forming the layers such that the total thickness of the first and second layers is 0.5-4.0 μm , and the total thickness of all layers is 2.0-6.0 μm .

15 **Brief Description of the Drawing Figures**

 Fig. 1 shows in 1800X magnification of a cross section of an insert according to the present invention.

Detailed Description of the Preferred Embodiments

 A cutting tool insert according to the invention useful for severing or
20 grooving of steel and stainless steel includes a cemented carbide substrate with a highly W-alloyed binder phase and with a well balanced chemical composition and grain size of the WC, a columnar $\text{TiC}_x\text{N}_y\text{O}_z$ -layer which layer thickness should be kept as low as possible, a $\kappa\text{-Al}_2\text{O}_3$ -layer, a TiN-layer and optionally followed by smoothening the cutting edges. For example, the edges may be smoothed by
25 brushing, e.g. - by a SiC-based brush. Surprisingly, beneficial properties have been achieved with a relatively thin coating.

The cobalt binder phase is highly alloyed with W. The content of W in the binder phase can be expressed as the CW-ratio = $M_s / (\text{wt\% Co} \cdot 0.0161)$, where M_s is the measured saturation magnetisation of the cemented carbide substrate in kA/m and wt% Co is the weight percentage of Co in the cemented carbide. The CW-value is a function of the W content in the Co binder phase. A low CW-value corresponds to a high W-content in the binder phase. According to the present invention improved cutting performance is achieved if the cemented carbide substrate has a CW-ratio of 0.78-0.93.

According to the present invention a parting tool insert is provided with a cemented carbide substrate with a composition of 6-15 wt% Co, preferably 9-12 wt% Co, and most preferably 10-11 wt% Co. The composition further includes 0.2-1.8 wt% cubic carbides, preferably 0.4-1.8 wt% cubic carbides, most preferably 0.5-1.7 wt% cubic carbides, of the metals Ta, Nb and Ti and balance WC. The cemented carbide may also contain other carbides from elements from group IVb, Vb or VIb of the periodic table. The content of Ti is preferably on a level corresponding to a technical impurity. The preferred average grain size of the WC depend on the binder phase content. At a preferred composition of 10-11 wt-% Co, the preferred grain size is 1.5-2.0 μm , most preferably about 1.7 μm . The CW-ratio shall be 0.78-0.93, preferably 0.80-0.91, and most preferably 0.82-0.90. The cemented carbide may contain small amounts, < 1 volume %, of η -phase (M_6C), without any detrimental effect. From the CW-value it follows that no free graphite is allowed in the cemented carbide substrate according to the present embodiment.

The coating comprises a first innermost layer of $\text{TiC}_x\text{N}_y\text{O}_z$ with $x+y+z=1$, preferably $y > x$ and $z < 0.2$, most preferably $y > 0.8$ and $z=0$, with equiaxed grains with a size < 0.5 μm , and a total thickness < 1.5 μm but > 0.1 μm , preferably the thickness is 0.1-0.6 μm ;

a second layer of $\text{TiC}_x\text{N}_y\text{O}_z$ with $x+y+z=1$, preferably with $z=0$, $x>0.3$ and $y>0.3$, most preferably $x>0.5$, with a thickness of $0.4\text{--}3.9\text{ }\mu\text{m}$, preferably the thickness is $1.5\text{--}3.0\text{ }\mu\text{m}$, the second layer has columnar grains with an average diameter of $<5\text{ }\mu\text{m}$, preferably $0.1\text{--}2.0\text{ }\mu\text{m}$;

5 the total thickness of the first and second layers is $0.5\text{--}4.0\text{ }\mu\text{m}$, preferably $1.5\text{--}3.5\text{ }\mu\text{m}$. Preferably, the first layer is thinner than the second layer;

a third layer of a smooth, fine-grained Al_2O_3 consisting essentially of the κ -phase having a grain size about $0.5\text{--}2\text{ }\mu\text{m}$. However, the layer may contain small amounts, 1-3 vol-%, of the θ or the α -phases as determined by x-ray
10 diffraction (XRD) measurement. The Al_2O_3 -layer has a thickness of $0.5\text{--}5.5\text{ }\mu\text{m}$, preferably $0.5\text{--}3.0\text{ }\mu\text{m}$;

preferably, this Al_2O_3 -layer is followed by a further layer of TiN having a thickness $<1\text{ }\mu\text{m}$, preferably $0.1\text{--}0.5\text{ }\mu\text{m}$ thick. The Al_2O_3 or the TiN layer can be the outermost layer. This outermost layer, whether Al_2O_3 or TiN, has a
15 surface roughness $R_{\text{max}}<0.4\text{ }\mu\text{m}$ over a length of $10\text{ }\mu\text{m}$. The TiN-layer, if present, is preferably removed along the cutting edge by a suitable removal technique, such as brushing; and

the total thickness of the first, second and third layers is $2\text{--}6\text{ }\mu\text{m}$, preferably $3\text{--}5\text{ }\mu\text{m}$.

20 According to a method of the invention, a WC-Co-based cemented carbide substrate is made with a highly W-alloyed binder phase with a CW-ratio of $0.78\text{--}0.93$, preferably $0.80\text{--}0.91$, and most preferably $0.82\text{--}0.90$. The content of cubic carbides of the metals Ta, Nb and Ti is $0.2\text{--}1.8\text{ wt}\%$, preferably $0.4\text{--}1.8\text{ wt}\%$, and most preferably $0.5\text{--}1.7\text{ wt}\%$. The substrate further includes $6\text{--}15\text{ wt}\%$ Co,
25 preferably $9\text{--}12\text{ wt}\%$ Co, and most preferably $10\text{--}11\text{ wt}\%$ Co. The WC grain size is $1.5\text{--}2.0\text{ }\mu\text{m}$, most preferably about $1.7\text{ }\mu\text{m}$, when the Co content is in the $10\text{--}11\text{ wt}\%$ range. The body is coated by:

a first innermost layer of $\text{TiC}_x\text{N}_y\text{O}_z$ with $x+y+z=1$, preferably $y > x$ and $z < 0.2$, most preferably $y > 0.8$ and $z = 0$, with equiaxed grains with size $< 0.5 \mu\text{m}$ and a total thickness $< 1.5 \mu\text{m}$, preferably $> 0.1 \mu\text{m}$, preferably $0.1-0.6 \mu\text{m}$, using known CVD-methods;

- 5 a second layer of $\text{TiC}_x\text{N}_y\text{O}_z$ with $x+y+z=1$, preferably with $z=0$, $x > 0.3$ and $y > 0.3$, most preferably $x > 0.5$, with a thickness of $0.4-3.9 \mu\text{m}$, preferably $1.5-3.0 \mu\text{m}$, with columnar grains and with an average diameter of about $< 5 \mu\text{m}$, preferably $0.1-2.0 \mu\text{m}$, is applied preferably using a MTCVD-technique (e.g. - using acetonitrile as the carbon and nitrogen source for forming the layer in the temperature range of $700-900^\circ\text{C}$). The exact conditions, however, depend to a certain extent on the design of the equipment used;

the total thickness of the first and second layers is $0.5-4.0 \mu\text{m}$, preferably $1.5-3.5 \mu\text{m}$. Preferably, the first layer is thinner than the second layer;

- 15 a third layer of a smooth, fine-grained Al_2O_3 consisting essentially of the κ -phase having a grain size about $0.5-2.0 \mu\text{m}$. The Al_2O_3 -layer has a thickness of $0.5-5.5 \mu\text{m}$, preferably $0.5-3.0 \mu\text{m}$. Preferably, this Al_2O_3 -layer is followed by a further layer of TiN having a thickness $< 1 \mu\text{m}$, preferably $0.1-0.5 \mu\text{m}$ thick. The Al_2O_3 layer can be exposed as the outermost layer. The outermost layer of Al_2O_3 or TiN has a surface roughness $R_{\text{max}} < 0.4 \mu\text{m}$ over a length of $10.0 \mu\text{m}$. The smooth coating surface can be obtained by gently wet-blasting the coating surface with fine grained (400-150 mesh) alumina powder, or by brushing (preferably used when TiN top layer is present) the edges with brushes based on SiC as disclosed in Swedish patent application 9402543-4. The TiN -layer, if present, is preferably removed along the cutting edge; and

- 25 the total thickness of the first, second and third layers is $2.0-6.0 \mu\text{m}$, preferably $3.0-5.0 \mu\text{m}$.

As a way of further illustrating the present invention and the advantages thereof, the following examples are given.

Example 1

A. A cemented carbide cutting tool insert in style N151.2-300-5E with the composition 10.5 wt-% Co, 1.16 wt-% Ta, 0.28 wt-% Nb and balance WC, with a binder phase highly alloyed with W corresponding to a CW-ratio of 0.87, was coated with an innermost 0.5 μm equiaxed $\text{TiC}_{0.05}\text{N}_{0.95}$ -layer with a high nitrogen content, corresponding to an estimated C/N ratio of 0.05, followed by a 2.2 μm thick layer of columnar $\text{TiC}_{0.54}\text{N}_{0.46}$ deposited using MT-CVD technique. In subsequent steps during the same coating process a 1.5 μm layer of Al_2O_3 consisting of pure κ -phase was formed according to procedure disclosed in EP-A-523 021. A thin, 0.5 μm , TiN layer was deposited, during the same cycle, on top of the Al_2O_3 -layer. Hence, the total thickness of all layers is 4.7 μm . The coated insert was brushed by a SiC containing nylon straw brush after coating, removing the outer TiN layer on the edge.

B. A cemented carbide cutting tool insert in style N151.2-300-SE with the composition of 8.0 wt-% Co, no cubic carbides, balance WC and a CW-ratio of 0.94 was prepared. The insert was coated with an innermost 0.5 μm equiaxed TiCN-layer. A 1.5 μm TiN layer was deposited, during the same cycle, on top of the TiCN-layer. No post treatment was applied.

C. A cemented carbide cutting tool insert in style N151.2-300-5E with the composition of 8.0 wt-% Co, no cubic carbides, balance WC and a CW-ratio of 0.94. The insert was coated with an innermost 0.5 μm equiaxed TiCN-layer with a high nitrogen content, corresponding to an estimated C/N ratio of 0.05, followed by a 4.0 μm thick layer of columnar TiCN deposited using MT-CVD technique. In subsequent steps during the same coating process a 1.0 μm layer of Al_2O_3 consisting of pure κ phase was formed according to procedure disclosed in EP-A-523-021. A thin, 0.5 μm TiN layer was deposited, during the same cycle, on top of the Al_2O_3 -layer. The coated insert was brushed by a SiC containing nylon straw brush after coating, removing the outer TiN layer on the edge.

D. A comparative cemented carbide cutting tool insert in style similar to N151.2-300-5E from an external leading cemented carbide producer was selected for comparison. The carbide had a composition of 11.0 wt-% Co, 7.1 wt-% TiC, 12.1 wt-% TaC, 1.3 wt-% NbC, balance WC and a CW-ratio of 0.80. The insert had a coating consisting of 1.1 μm TiN and, outermost, 0.3 μm TiCN layer. Examination in light optical microscope revealed no edge treatment subsequent to coating.

Inserts from A, B and C were compared in a flaking test comprising a facing operation in austenitic stainless steel (SanMac 304L). Feed 0.15 mm/rev, speed 130 m/min and depth of cut varying between 0-2.5 mm.

Insert	Number of cuts before extensive flaking
A (acc. to invention)	10
B (outside invention)	5
C (outside invention)	1
D (external grade)	1

Example 2

Inserts A, B, C and D from above were tested in a severing test of stainless steel (SS2343) in the form of 12mm bar stainless steel.

The rotating speed was 1800 rpm, feed varying 0.15-0.02 mm/rev (low feed rate close to centre of bar).

The wear mechanism was flaking combined with nose cracking.

	Insert	Number of components
	A (acc. to invent.)	380
	B (outside invention)	180
	C (outside invention)	200
5	D (external grade)	200

Example 3

Inserts A (insert style N151.2-400-4E) and D were tested at an end users machine shop in severing of a stainless steel tube (SS2343, OD 27mm, ID 25mm) with feed 0.05 mm/rev and speed 150 m/min.

- 10 Insert D failed due to major chipping of the cutting edge while a very small chipping was seen on insert A.

Insert	Number of components
A (acc. to invention)	324
D (external grade)	108

15 Example 4

Inserts A and D were tested at an end users machine shop in parting to centre of an annealed high alloy steel SS2242 with feed 0.15 mm/rev and speed 100 m/min.

- 20 Insert D failed due to cracking in the corners while a very small deformation in the corners was seen on insert A.

Insert	Number of components
A (acc. to invention)	400
D (external grade)	150

Example 5

Inserts A (insert style N151.2-400-4E) and D were tested at an end users machine shop in parting of a steel bar (SS2225, OD 50mm) with feed 0.06-0.14 mm/rev and speed 180 m/min.

- 5 Insert D failed due to chipping of the cutting edge while even flank wear was seen on insert A.

Insert	Number of components
A (acc. to invention)	300
D (external grade)	150

- 10 While the present invention has been described by reference to the above-described embodiments, certain modifications and variations will be evident to those of ordinary skill in the art. Therefore, the present invention is to limited only the scope and spirit of the appended claims.

What is claimed is:

1 1. A cutting tool insert comprising:
2 a cemented carbide body comprising
3 6-15 weight % Co, 0.2-1.8 weight % cubic carbides of Ti, Ta, Nb
4 or any combination thereof, a highly W-alloyed binder phase with a CW-
5 ratio of 0.78-0.93, and the balance WC; and
6 a coating comprising
7 a first innermost layer of $\text{TiC}_x\text{N}_y\text{O}_z$ wherein $x+y+z=1$, the first
8 layer having a thickness of 0.1-1.5 μm and equiaxed grains with size < 0.5
9 μm ,
10 a second layer of $\text{TiC}_x\text{N}_y\text{O}_z$ wherein $x+y+z=1$, the second layer
11 having a thickness of 0.4-3.9 μm , with columnar grains with an average
12 diameter of 0.1-5.0 μm ,
13 a third layer of a smooth fine-grained $\kappa\text{-Al}_2\text{O}_3$ layer with a
14 thickness of 0.5-5.5 μm , and
15 a total thickness of the first innermost $\text{TiC}_x\text{N}_y\text{O}_z$ and the second
16 $\text{TiC}_x\text{N}_y\text{O}_z$ layer is 0.5-4.0 μm , and the total thickness of all layers is 2.0-
17 6.0 μm .

1 2. The cutting tool insert of claim 1, wherein the body comprises 9-12
2 weight % Co and a CW ratio of 0.80-0.91.

1 3. The cutting tool inset of claim 1, wherein in the first layer $y > x$ and
2 $z < 0.2$, and the thickness of the first layer is 0.1-0.6 μm .

1 4. The cutting tool insert of claim 1, wherein in the second layer $z=0$,
2 $x > 0.3$ and $y > 0.3$, the second layer has a thickness of 1.5-3.0 μm , with the
3 columnar grains having an average diameter of 0.1-2.0 μm .

1 5. The cutting tool insert of claim 1, wherein in the third layer the grains
2 of the $\kappa\text{-Al}_2\text{O}_3$ have a size on the order of 0.5-2.0 μm , and the third layer has a
3 thickness of 0.5-3.0 μm .

1 6. The cutting tool insert of claim 1, wherein the total thickness of the first
2 and second layers is 1.5-3.5 μm .

1 7. The cutting tool insert of claim 1, wherein the total thickness of all the
2 layers is 3.0-5.0 μm .

1 8. The cutting insert of claim 1 further comprising an outermost layer of
2 TiN having a thickness of 0.1-1.0 μm .

1 9. The cutting insert of claim 8, wherein the outermost TiN-layer has been
2 removed along the cutting edge.

1 10. A method of making a cutting tool insert comprising a WC-Co-based
2 cemented carbide body with a highly W-alloyed binder phase and a CW-ratio of
3 0.78-0.93, the method comprising coating the body by the steps of:

4 forming a first innermost layer of $\text{TiC}_x\text{N}_y\text{O}_z$ with a CVD-based technique,
5 wherein $x+y+z=1$, the first layer having a thickness of 0.1-1.5 μm and equiaxed
6 grains with a size $< 0.5 \mu\text{m}$,

7 forming a second layer of $\text{TiC}_x\text{N}_y\text{O}_z$ by a MTCVD-technique, wherein
8 $x+y+z=1$, the second layer having a thickness of 0.4-3.9 μm and columnar grains
9 with an average diameter of 0.1-5.0 μm ,

10 forming a third layer of a smooth $\kappa\text{-Al}_2\text{O}_3$ having a thickness of 0.5-5.5
11 μm , and

12 forming the layers such that the total thickness of the first and second
13 layers is 0.5-4.0 μm , and the total thickness of all layers is 2.0-6.0 μm .

1 11. The method of claim 10, wherein the step of forming the first layer
2 further comprises providing the first layer with $y > x$ and $z < 0.2$ and a thickness
3 of 0.1-0.6 μm .

1 12. The method of claim 10 wherein the step of forming the second layer
2 further comprises using acetonitrile as the carbon and nitrogen source and forming
3 the second layer at a temperature of 850-900°C, the step of forming the second
4 layer further comprises providing $z=0$, $x > 0.3$ and $y > 0.3$, a thickness of 1.5-3.0
5 μm , and with the columnar grains having an average diameter of 0.1-2.0 μm .

1 13. The method of claim 10, wherein the third layer is provided with a
2 thickness of 0.5-3.0 μm .

1 14. The method of claim 10, wherein the method further comprises
2 forming an outer layer of TiN having a thickness of $< 1\mu\text{m}$.

1 15. The method of claim 10, wherein the method further comprises
2 providing the first and second layers with a total thickness of 1.5-3.5 μm , and a
3 total thickness of all layers of 3.0-5.0 μm .

1 16. The method of claim 10 wherein the said cemented carbide body has a
2 cobalt content of 9-12 weight % and 0.4-1.8 weight % cubic carbides of Ta and
3 Nb.

1 17. The method of claim 10 wherein the cemented carbide body has a
2 cobalt content of 10-11 weight %.

1 18. The method of claim 17 wherein the cemented carbide body has a CW-
2 ratio of 0.82-0.90.

1 19. The method of claim 14, wherein the outermost TiN-layer is removed
2 along a cutting edge.

1 20. The method of claim 19, wherein the outermost TiN-layer is removed
2 by brushing.

Abstract of the Disclosure

The present invention relates to a coated cutting tool insert useful for grooving or severing steel components such as steel or stainless steel tubes and bars. The insert is characterised by WC-Co-based cemented carbide substrate having a highly W-alloyed Co-binder phase and a relatively thin coating including an inner layer of $\text{TiC}_x\text{N}_y\text{O}_z$ with columnar grains followed by a layer of fine grained $\kappa\text{-Al}_2\text{O}_3$ and a top layer of TiN.

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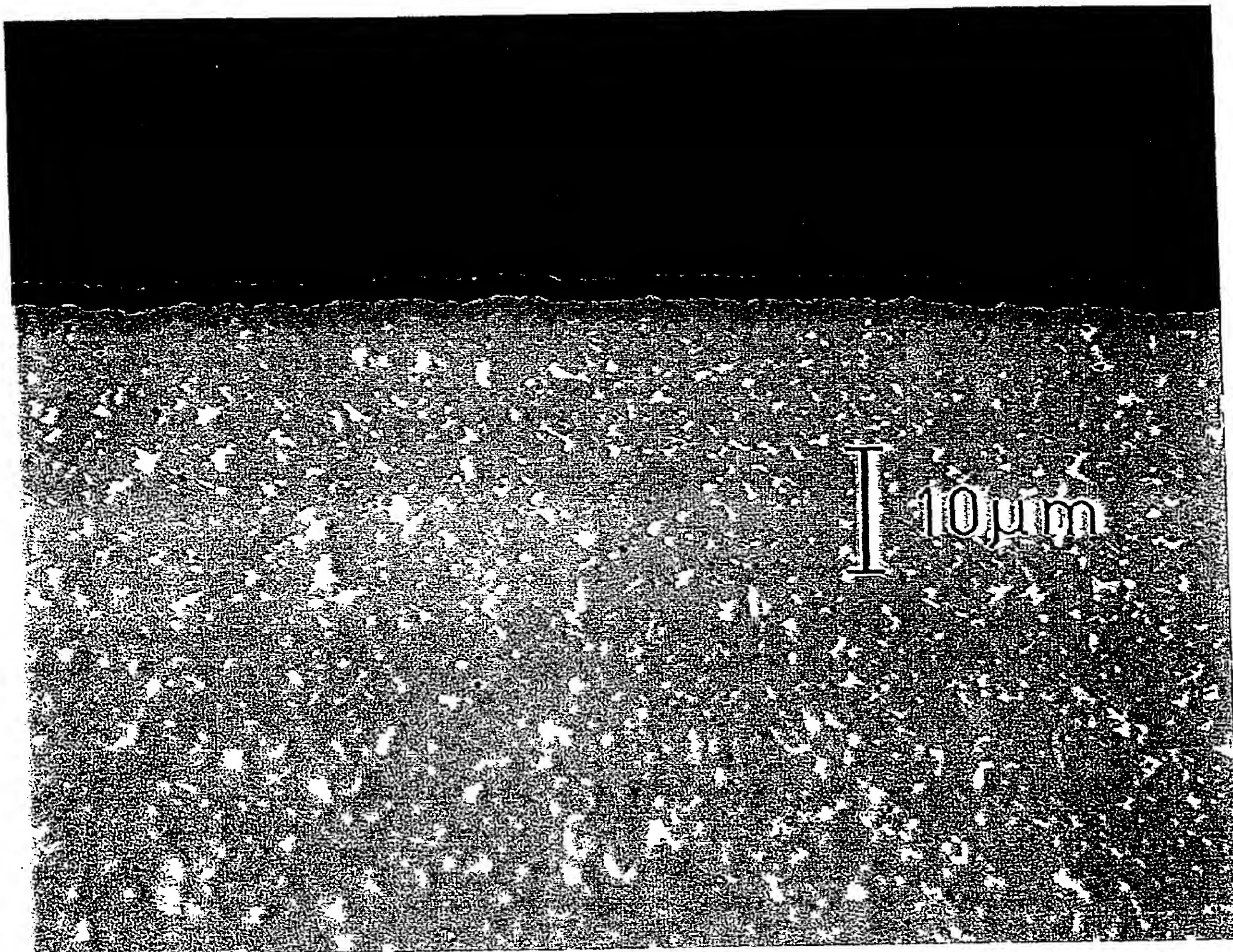


Fig. 1

**COMBINED DECLARATION AND POWER OF ATTORNEY
FOR UTILITY PATENT APPLICATION**

Attorney's Docket No.
024444-638

As a below-named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below next to my name;

I BELIEVE I AM THE ORIGINAL, FIRST AND SOLE INVENTOR (if only one name is listed below) OR AN ORIGINAL, FIRST AND JOINT INVENTOR (if more than one name is listed below) OF THE SUBJECT MATTER WHICH IS CLAIMED AND FOR WHICH A PATENT IS SOUGHT ON THE INVENTION ENTITLED:

COATED GROOVING OR PARTING INSERT

the specification of which

(check one)

☐

is attached hereto;

☒

was filed on July 8, 1999 as

Application No. _____

and was amended on _____;
(if applicable)

I HAVE REVIEWED AND UNDERSTAND THE CONTENTS OF THE ABOVE-IDENTIFIED SPECIFICATION, INCLUDING THE CLAIMS, AS AMENDED BY ANY AMENDMENT REFERRED TO ABOVE;

I ACKNOWLEDGE THE DUTY TO DISCLOSE TO THE OFFICE ALL INFORMATION KNOWN TO ME TO BE MATERIAL TO PATENTABILITY AS DEFINED IN TITLE 37, CODE OF FEDERAL REGULATIONS, Sec. 1.56 (as amended effective March 16, 1992);

I do not know and do not believe the said invention was ever known or used in the United States of America before my or our invention thereof, or patented or described in any printed publication in any country before my or our invention thereof or more than one year prior to said application; that said invention was not in public use or on sale in the United States of America more than one year prior to said application; that said invention has not been patented or made the subject of an inventor's certificate issued before the date of said application in any country foreign to the United States of America on any application filed by me or my legal representatives or assigns more than twelve months prior to said application;

I hereby claim foreign priority benefits under Title 35, United States Code Sec. 119 and/or Sec. 365 of any foreign application(s) for patent or inventor's certificate as indicated below and have also identified below any foreign application for patent or inventor's certificate on this invention having a filing date before that of the application(s) on which priority is claimed:

COMBINED DECLARATION AND POWER OF ATTORNEY			Attorney's Docket No. 024444-638																																																																																					
COUNTRY/INTERNATIONAL	APPLICATION NUMBER	DATE OF FILING (day, month, year)	PRIORITY CLAIMED																																																																																					
SWEDEN	9802488-8	9/JULY/1998	YES <u>X</u> NO <u> </u>																																																																																					
			YES <u> </u> NO <u> </u>																																																																																					
<p>I hereby appoint the following attorneys and agent(s) to prosecute said application and to transact all business in the Patent and Trademark Office connected therewith and to file, prosecute and to transact all business in connection with international applications directed to said invention:</p> <table style="width: 100%; border: none;"> <tr> <td style="width: 33%;">William L. Mathis</td> <td style="width: 10%; text-align: right;">17,337</td> <td style="width: 33%;">R. Danny Huntington</td> <td style="width: 10%; text-align: right;">27,903</td> <td style="width: 33%;">Gerald F. Swiss</td> <td style="width: 10%; text-align: right;">30,113</td> </tr> <tr> <td>Robert S. Swecker</td> <td style="text-align: right;">19,885</td> <td>Eric H. Weisblatt</td> <td style="text-align: right;">30,505</td> <td>Michael J. Ure</td> <td style="text-align: right;">33,089</td> </tr> <tr> <td>Platon N. Mandros</td> <td style="text-align: right;">22,124</td> <td>James W. Peterson</td> <td style="text-align: right;">26,057</td> <td>Charles F. Wieland III</td> <td style="text-align: right;">33,096</td> </tr> <tr> <td>Benton S. Duffett, Jr.</td> <td style="text-align: right;">22,030</td> <td>Teresa Stanek Rea</td> <td style="text-align: right;">30,427</td> <td>Bruce T. Wieder</td> <td style="text-align: right;">33,815</td> </tr> <tr> <td>Norman H. Stepno</td> <td style="text-align: right;">22,716</td> <td>Robert E. Krebs</td> <td style="text-align: right;">25,885</td> <td>Todd R. Walters</td> <td style="text-align: right;">34,040</td> </tr> <tr> <td>Ronald L. Grudziecki</td> <td style="text-align: right;">24,970</td> <td>William C. Rowland</td> <td style="text-align: right;">30,888</td> <td>Ronni S. Jillions</td> <td style="text-align: right;">31,979</td> </tr> <tr> <td>Frederick G. Michaud, Jr.</td> <td style="text-align: right;">26,003</td> <td>T. Gene Dillahunt</td> <td style="text-align: right;">25,423</td> <td>Harold R. Brown III</td> <td style="text-align: right;">36,341</td> </tr> <tr> <td>Alan E. Kopecki</td> <td style="text-align: right;">25,813</td> <td>Patrick C. Keane</td> <td style="text-align: right;">32,858</td> <td>Allen R. Baum</td> <td style="text-align: right;">36,086</td> </tr> <tr> <td>Regis E. Slutter</td> <td style="text-align: right;">26,999</td> <td>Bruce J. Boggs, Jr.</td> <td style="text-align: right;">32,344</td> <td>Steven M. du Bois</td> <td style="text-align: right;">35,023</td> </tr> <tr> <td>Samuel C. Miller III</td> <td style="text-align: right;">27,360</td> <td>William H. Benz</td> <td style="text-align: right;">25,952</td> <td>Brian P. O'Shaughnessy</td> <td style="text-align: right;">32,747</td> </tr> <tr> <td>Robert G. Mukai</td> <td style="text-align: right;">28,531</td> <td>Peter K. Skiff</td> <td style="text-align: right;">31,917</td> <td> </td> <td> </td> </tr> <tr> <td>George A. Hovanec, Jr.</td> <td style="text-align: right;">28,223</td> <td>Richard J. McGrath</td> <td style="text-align: right;">29,195</td> <td> </td> <td> </td> </tr> <tr> <td>James A. LaBarre</td> <td style="text-align: right;">28,632</td> <td>Matthew L. Schneider</td> <td style="text-align: right;">32,814</td> <td> </td> <td> </td> </tr> <tr> <td>E. Joseph Gess</td> <td style="text-align: right;">28,510</td> <td>Michael G. Savage</td> <td style="text-align: right;">32,596</td> <td> </td> <td> </td> </tr> </table>					William L. Mathis	17,337	R. Danny Huntington	27,903	Gerald F. Swiss	30,113	Robert S. Swecker	19,885	Eric H. Weisblatt	30,505	Michael J. Ure	33,089	Platon N. Mandros	22,124	James W. Peterson	26,057	Charles F. Wieland III	33,096	Benton S. Duffett, Jr.	22,030	Teresa Stanek Rea	30,427	Bruce T. Wieder	33,815	Norman H. Stepno	22,716	Robert E. Krebs	25,885	Todd R. Walters	34,040	Ronald L. Grudziecki	24,970	William C. Rowland	30,888	Ronni S. Jillions	31,979	Frederick G. Michaud, Jr.	26,003	T. Gene Dillahunt	25,423	Harold R. Brown III	36,341	Alan E. Kopecki	25,813	Patrick C. Keane	32,858	Allen R. Baum	36,086	Regis E. Slutter	26,999	Bruce J. Boggs, Jr.	32,344	Steven M. du Bois	35,023	Samuel C. Miller III	27,360	William H. Benz	25,952	Brian P. O'Shaughnessy	32,747	Robert G. Mukai	28,531	Peter K. Skiff	31,917			George A. Hovanec, Jr.	28,223	Richard J. McGrath	29,195			James A. LaBarre	28,632	Matthew L. Schneider	32,814			E. Joseph Gess	28,510	Michael G. Savage	32,596		
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I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.																																																																																								
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COMBINED DECLARATION AND POWER OF ATTORNEY		Attorney's Docket No. 024444-638	
FULL NAME OF FOURTH JOINT INVENTOR, IF ANY Gregor KULLANDER		SIGNATURE	
RESIDENCE Långsjöhöjden 79, 125 51 Älvsjö, SWEDEN		CITIZENSHIP SWEDEN	
POST OFFICE ADDRESS (same as above)			
FULL NAME OF FIFTH JOINT INVENTOR, IF ANY		SIGNATURE	
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FULL NAME OF SIXTH JOINT INVENTOR, IF ANY		SIGNATURE	
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FULL NAME OF SEVENTH JOINT INVENTOR, IF ANY		SIGNATURE	
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